GENERATOR INTERCONNECTION SYSTEM IMPACT STUDY REPORT

for integration of the proposed

3 MW

IPC PROJECT QUEUE #525

to the

IDAHO POWER COMPANY ELECTRICAL SYSTEM

for

REPORT v.0

October 17, 2017

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Revision History

Date	Revision	Initials	Summary of Changes
10/17/2017	0	PMA	SISR GI #525 – Original issue.

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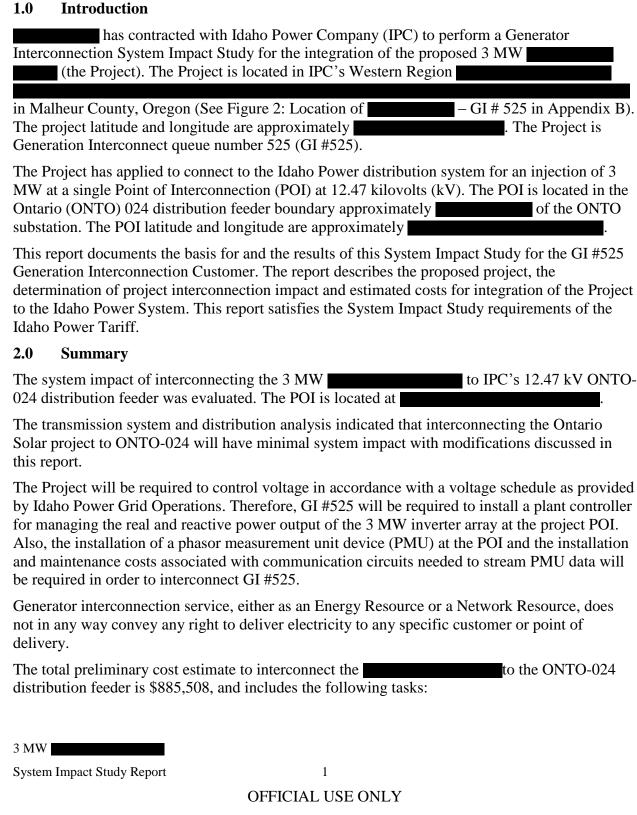
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- Install a four-pole 12.47 kV generation interconnection package at the POI. This includes an SEL-421 protective relay, which requires 3-phase potential transformers (PTs), 3-phase current transformers (CTs), and remote connectivity. Additionally, a single-phase PT shall be installed on the interconnect customer side of the IPC recloser.
- Reconductor approximately 2.25 miles from the POI from #4 ACSR to 795 AAC.
- Replace recloser ONTO24R70X with an electronic recloser. Additionally, a single-phase PT shall be installed on the interconnect customer side of the recloser for deadline check.
- Install a PMU device at the POI.
- Install a single-phase PT and wiring for dead-line check on ONTO-024.
- Install Beckwith M2001-D load tap changer (LTC) controllers on the T134 transformer at ONTO substation.
- Upgrade the ONTO T022 AMI transformer.

The cost estimate includes direct equipment and installation labor costs, indirect labor costs and general overheads, and a contingency allowance. These are cost estimates only and final charges to the customer will be based on the actual construction costs incurred. It should be noted that the preliminary cost estimate of \$885,508 does not include the cost of the customer's owned equipment to construct the solar generation site or required communication circuits.

3.0 Scope of Interconnection Transmission System Impact Study

The Interconnection Transmission System Impact Study was completed, in accordance with Idaho Power Company Standard Generator Interconnection Procedures, to provide an evaluation of the system impacts of the interconnection of the proposed generating project to the Idaho Power system. As listed in the Interconnection Transmission System Impact Study agreement, the Interconnection Transmission System Impact Study report provides the following information:

- identification of additional transformer load tap changer operations, voltage fluctuations (flicker) and additional feeder losses.
- identification of required reactive power support.
- identification of islanding conditions.
- identification of any circuit breaker short circuit capability limits exceeded as a result of the interconnection.
- identification of any thermal overload or voltage limit violations resulting from the interconnection.
- identification of any angular instability.
- description and non-binding estimated cost of facilities required to interconnect the Small Generating Facility to the IPC System and to address the identified short circuit and power flow issues.

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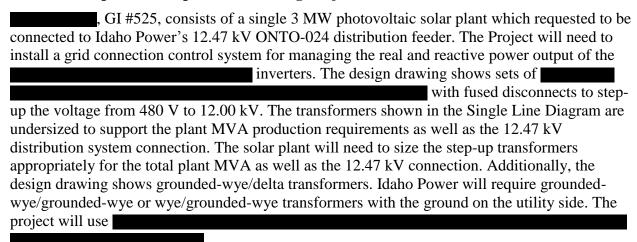
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All other proposed generation projects prior to this project in the Generator Interconnect queue were considered in this study. A current list of these projects can be found in the Generation Interconnection folder located on the Idaho Power web site at the link shown below:

http://www.oatioasis.com/ipco/index.html.

4.0 Description of Proposed Generating Project



The Project's projected in-service date was not included in the GI application.

5.0 Description of Transmission Facilities

The Project's impact on the Brownlee East transmission path (WECC Path #55) was evaluated in this Transmission System Impact Study. In addition, the Idaho-Northwest transmission path (WECC Path #14) which is in series with the Brownlee East transmission path was studied at its rated West-to-East transfer capacity.

The Idaho-Northwest transmission path (WECC Path #14) is defined as the sum of the flows on the following five lines:

- Oxbow-Lolo 230kV
- Hells Canyon-Hurricane 230kV
- North Powder-La Grande 230kV
- Hines-Harney 115kV
- Hemingway-Summer Lake 500kV

The Brownlee East transmission path (WECC Path #55) is defined as the sum of the flows on the following seven lines:

- Brownlee-Boise Bench #1 230kV
- Brownlee-Boise Bench #2 230kV

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- Brownlee-Boise Bench #3 230kV
- Brownlee-Horse Flat #4 230kV
- Brownlee-Ontario 230kV
- Oxbow-Starkey 138kV
- Quartz-Ontario 138kV

For this generation interconnection Transmission System Impact Study, the flow on the Idaho-Northwest transmission path was modeled at MW West-to-East and the Brownlee East transmission path was modeled at MW West-to-East. The paths were stressed to these specific levels in order to determine if the addition of the Project's 3 MW degraded the existing Brownlee East path's transfer capability.

6.0 Description of Power Flow Case

This study utilized the WECC approved 16hs3a Heavy summer operating case as the starting point of the studies. Two power flow cases were developed:

- The "Base Case" with projects earlier in the queue added, but not the Project.
- The "Second Case" with projects earlier in the queue and the Project added.

The pre-contingency flows across the Idaho-Northwest and the Brownlee East paths/cut-planes were modeled at their respective ratings (see Section 5.0). Flow in each path is modeled in this manner in order to capture the potential impact of the Project on the existing capabilities of the surrounding paths and the interconnected transmission systems. Performing the studies at these levels will ensure that the Total Transfer Capability of the adjacent paths are not impacted by the Project.

In addition to the 16hs3a Heavy summer operating case, two light-load operating cases were developed for the IPC 69 kV sub-transmission system. The limits used for this analysis are as follows:

- 1. Voltage magnitude during normal operating steady-state must remain between 0.93 per unit and 1.05 per unit. If the post-transient voltage deviates from this range during N-1 conditions and an operating procedure can be taken to return the voltage to the required range without creating a four-terminal line, then network upgrades are not required.
- 2. Line loading must be less than 100% of line rating during normal steady-state operation. Steady-state line loading above 100% requires network upgrades.
- 3. Post-transient line overloading that does not exceed the emergency line rating resulting from an N-1 contingency is acceptable if an operating procedure can be taken to reduce the line loading below 100% without creating a four-terminal line.
- 4. Post-transient line loading above the emergency line rating resulting from an N-1 contingency requires network upgrades.

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7.0 Power Flow Analysis Study Results

Results from the stressed Heavy summer operating case indicate the addition of the GI #525 project will not result in contingency violations that would impact the Total Transfer Capability of the adjacent Brownlee East transmission path.

The addition of GI #525 does not exceed any lines ratings for any N-1 contingencies.

8.0 Description of Substation Facilities

Idaho Power's ONTO substation is located in Malheur County, Oregon. The existing substation transformer, ONTO T134, is a three-phase 138-13.09 kV transformer rated for 30 MVA.

9.0 Description of Distribution Facilities

The requested POI for the Project is on the ONTO-024 distribution feeder. This is a grounded-wye feeder operating at 12.47 kV at the POI. The Project must have a grounded-wye transformer connection on the IPC side, as well as a wye connection on the Project side of the transformer.

Refer to Appendix A, Section 3, for additional grounding requirements.

10.0 Short Circuit Study Results

The fault current contribution from the PV generators does not exceed any circuit breaker rating.

11.0 Description of Required Facility Upgrades

The Project will be required to provide a plant controller that will operate the inverter system in Volt/VAr control mode in order to regulate voltage according to a voltage schedule that will be provided by Idaho Power.

The following upgrades will be required to IPC-owned facilities to facilitate the interconnection of GI #525:

- Install a four-pole 12.47 kV generation interconnection package at the POI. This includes an SEL-421 protective relay, which requires 3-phase potential transformers (PTs), 3-phase current transformers (CTs), and remote connectivity. Additionally, a single-phase PT shall be installed on the interconnect customer side of the IPC recloser.
- Reconductor approximately 2.25 miles from the POI from #4 ACSR to 795 AAC.
- Replace recloser ONTO24R70X with an electronic recloser. Additionally, a single-phase PT shall be installed on the interconnect customer side of the recloser for deadline check.
- Install a PMU device at the POI.
- Install a single-phase PT and wiring for dead-line check on ONTO-024.
- Install Beckwith M2001-D load tap changer (LTC) controllers on the T134 transformer at ONTO substation.

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• Upgrade the ONTO T022 AMI transformer.

See the conceptual-level cost estimate in Table 1.

Table 1 Conceptual-level Cost Estimate for GI #525

Item of Work	Estimate
Generation interconnection and protection package	\$174,000
Substation upgrades	\$5,800
Distribution upgrades	\$464,000
Unloaded costs	643,800
Contingency 20% (1)	\$128,760
Total unloaded costs	\$772,560
Overheads (2)	\$112,948
Total loaded costs	\$885,508
Total Conceptual-level Cost Estimate in 2017 dollars (3)	\$885,508

⁽¹⁾ Contingency is added to cover the unforeseen costs in the estimate. These costs can include unidentified design components, material cost increases, labor estimate shortfalls, etc.

- Note that these estimates do not include the cost of the customer's equipment/facilities or required communication circuits for SCADA, PMU, and metering.
- Note that the overhead rates are subject to change during the year.
- These are estimated costs only and final charges to the customer will be based on the actual construction costs incurred.
- These are non-binding conceptual level cost estimates that will be further refined upon the request and completion of Transmission and Distribution Facility Studies.

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⁽²⁾ Overhead costs cover the indirect costs associated with the Project.

⁽³⁾ This cost estimate includes direct equipment, material, labor, overheads, and contingency as shown.

12.0 Description of Operating Requirements

The Project shall be capable of injecting reactive power (over-excited) and absorbing reactive power (under-excited) equal to 1.45 MVAR at all active power output between 20% and 100% of the nameplate active power rating of 3 MW.

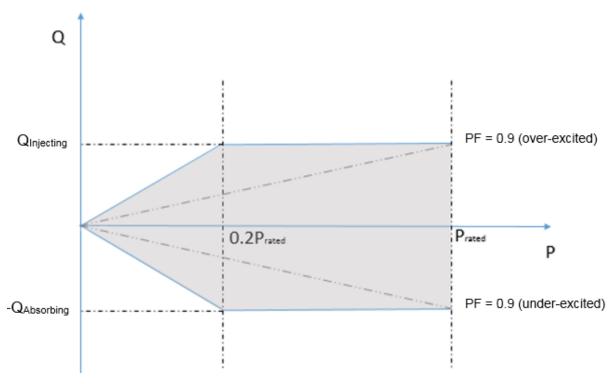


Figure 1 Operating requirements

Idaho Power has determined that the inverter selected by the Project meets the reactive power capability requirements.

The Project will be required to control voltage in accordance with a voltage schedule as provided by Idaho Power Grid Operations. Therefore, GI #525 will be required to install a plant controller for managing the real and reactive power output of the 3 MW inverter system at the project POI. The installation of a PMU at the POI and maintenance costs associated with communication circuits needed to stream PMU data will also be required in order to interconnect GI #525.

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Voltage flicker at startup and during operation will be limited to less than 5% as measured at the POI. The allowable voltage flicker limit is further reduced during operation due to multiple voltage fluctuations per hour or minute, per Idaho Power's T&D Advisory Information Manual.

The Project is required to comply with the applicable voltage fluctuation limits found in IEEE Standard 1453-2004 *IEEE Recommended Practice for Measurement and Limits of Voltage Fluctuations and Associated Light Flicker on AC Power Systems*.

The project is required to comply with the applicable Voltage and Current Distortion Limits found in IEEE Standard 519-2014 *IEEE Recommended Practices and Requirements for Harmonic Control in Electrical Power Systems*.

Additional operating requirements for the Project may be identified in the System Impact Study when it is performed.

13.0 Conclusion

The requested interconnection of the GI #525, to Idaho Power's system was studied for impact to the IPC electrical transmission and distribution system. The project will need to interconnect using a 12.47 kV grounded-wye connection to the ONTO-024 12.47 kV distribution feeder. The transformers shown in the Single Line Diagram are undersized to support the plant MVA production requirements as well as the 12.47 kV distribution system connection. The solar plant will need to size the step-up transformers appropriately for the total plant MVA as well as the 12.47 kV connection. Additionally, the design drawing shows grounded-wye/delta transformers. Idaho Power will require grounded-wye/grounded-wye or wye/grounded-wye transformers with the ground on the utility side. The results of this study confirm that, with the modifications listed, no network upgrades will be required to interconnect , GI #525, to the existing Idaho Power system. A four-pole generation interconnect package, a PMU, dead-line check, and a digital tap changer controls on the ONTO T134 are required to integrate the 3 MW project as well as reconductoring approximately 2.25 miles from the POI from #4 ACSR to 795 AAC and replacing recloser ONTO24R70X with an electronic recloser. Additionally, a singlephase PT shall be installed on the interconnect customer side of ONTO24R70X for deadline check.

All generation projects in the area ahead of the Project in the IPC generation interconnection queue and their associated transmission system improvements were modeled in a preliminary power flow analysis to evaluate the feasibility of interconnecting GI #525. The results and conclusions of this System Impact Study are based on the realization of these projects in the unique queue/project order.

The estimated cost to interconnect GI #525 to the IPC system at the 12.47 kV point of interconnection considered in this study is approximately \$885,508.

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Generator interconnection service, either as an Energy Resource or a Network Resource, does not in any way convey any right to deliver electricity to any specific customer or point of delivery. Transmission requirements to integrate the Project will be determined during the System Impact Study phase of the generator interconnection process. 3 MW 9 System Impact Study Report OFFICIAL USE ONLY

APPENDIX A

A-1.0 Method of Study

The Transmission System Impact Study plan inserts the Project up to the maximum requested injection into the selected Western Electricity Coordinating Council (WECC) power flow case and then, using Power World Simulator or GE's Positive Sequence Load Flow (PSLF) analysis tool, examines the impacts of the new resource on Idaho Power's transmission system (lines, transformers, etc.) within the study area under various operating and outage scenarios. The WECC and Idaho Power reliability criteria and Idaho Power operating procedures were used to determine the acceptability of the configurations considered. The WECC case is a recent case modified to simulate stressed but reasonable pre-contingency energy transfers utilizing the IPC system. For distribution feeder analysis, Idaho Power utilizes DNV·GL's Synergi Electric software and EPRI's OpenDSS software.

A-2.0 Acceptability Criteria

The following acceptability criteria were used in the power flow analysis to determine under which system configuration modifications may be required:

The continuous rating of equipment is assumed to be the normal thermal rating of the equipment. This rating will be as determined by the manufacturer of the equipment or as determined by Idaho Power. Less than or equal to 100% of continuous rating is acceptable.

Idaho Power's Voltage Operating Guidelines were used to determine voltage requirements on the system. This states, in part, that distribution voltages, under normal operating conditions, are to be maintained within plus or minus 5% (0.05 per unit) of nominal at each meter or POI on the feeder. Therefore, voltages greater than or equal to 0.95 pu voltage and less than or equal to 1.05 pu voltage are acceptable.

Voltage flicker during the starting or stopping of the generator will be limited to less than 5% as measured at the POI. Allowable voltage flicker limit is further reduced during operation due to multiple voltage fluctuations per hour or minute, per Idaho Power's T&D Advisory Information Manual.

Idaho Power's Reliability Criteria for System Planning was used to determine proper transmission system operation.

All customer generation must meet IEEE 519, IEEE1453, IEEE1547, and ANSI C84.1 Standards.

All other applicable national and Idaho Power standards and prudent utility practices were used to determine the acceptability of the configurations considered.

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The stable operation of the system requires an adequate supply of volt-amperes reactive (VARs) to maintain a stable voltage profile under both steady-state and dynamic system conditions. An inadequate supply of VARs will result in voltage decay or even collapse under the worst conditions.

Equipment/line/path ratings used will be those that are in use at the time of the study or that are represented by IPC upgrade projects that are either currently under construction or whose budgets have been approved for construction in the near future. All other potential future ratings are outside the scope of this study. Future transmission changes may, however, affect current facility ratings used in the study.

A-3.0 Grounding Guidance

IPC requires interconnected transformers on the distribution system to limit their ground fault current to 20 amps at the Point of Interconnection.

A-4.0 Electrical System Protection Guidance

IPC requires electrical system protection per <u>Requirements for Generation Interconnections</u> found on the Idaho Power Web site,

http://www.idahopower.com/pdfs/BusinessToBusiness/facilityRequirements.pdf

A-5.0 WECC Coordinated Off-Nominal Frequency Load Shedding and Restoration Requirements

IPC requires frequency operational limits to adhere to WECC Under-frequency and Over-frequency Limits per the <u>WECC Coordinated Off-Nominal Frequency Load Shedding and Restoration Requirements</u> available upon request.

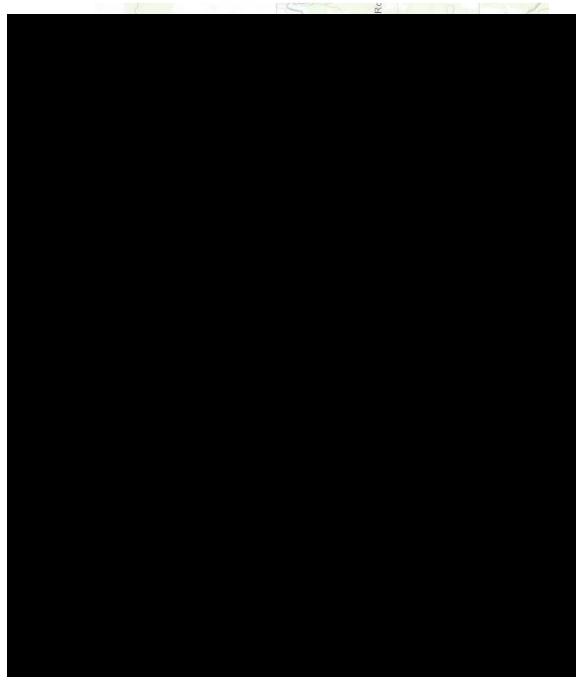
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APPENDIX B

B-1.0 GI Project #525 Site Location



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