# GENERATOR INTERCONNECTION FEASIBILITY STUDY REPORT

for integration of the proposed

**42 MW** 

**IPC PROJECT QUEUE #562** 

to the

#### IDAHO POWER COMPANY TRANSMISSION SYSTEM

for

**REPORT v.1** 

February, 2020

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# **Revision History**

Date	Revision	Initials	Summary of Changes
1/8/2020	0	AV	FeSR GI #562 – Original issue.
2/28/2020	1		Re-study due a senior project in the queue dropping out

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1.0 Introduction
has contracted with Idaho Power Company (IPC) to perform a Generator Interconnection Feasibility Study for the integration of the proposed 42 MW (the Project). The Project is to be located near Ontario in Malheur County, Oregon (See Figure 1 Location of Generation Interconnect queue number 562 (GI #562).
The Project has applied to connect to the Idaho Power transmission system for an injection of 42 MW at a single Point of Interconnection (POI) at 138 kilovolts (kV). The POI is on IPC's section of the approximately miles from IPC's station and approximately.
This report documents the basis for and the results of this feasibility study for the GI #562 Generation Interconnection Customer. The report describes the proposed project, the determination of project interconnection feasibility and estimated costs for integration of the Project to the Idaho Power System. This report satisfies the feasibility study requirements of the Idaho Power Tariff.
2.0 Summary
The feasibility of interconnecting the 42 MW to section of the section of the 138kV line was evaluated. The POI evaluated is approximately located at
The power flow analysis indicated that interconnecting the 42 MW section of the s
The Project will be assumed to

The Project will be required to control voltage in accordance with a voltage schedule as provided by Idaho Power Grid Operations. Therefore, GI #562 will be required to install a plant controller for managing the real and reactive power output of the 42 MW inverter array at the project POI. Also, the installation of phasor measurement unit devices (PMU's) at the POI and the maintenance costs associated with communication circuits needed to stream PMU data will be required to be provided to interconnect GI #562.

It is the generation project's responsibility to provide reactive power capability of the project to have a power factor operating range of at least 0.95 leading (absorbing) to at least 0.95 lagging (supplying) at the POI over the range of real power output up to maximum output of the project.

A Transmission System Impact Study is required to determine if any additional network upgrades are required to integrate the Project into the IPC transmission system and to evaluate system impacts such as thermal, voltage, transient stability, and reactive margin. Generator interconnection service, either as an Energy Resource or a Network Resource, does not in any way convey any right to deliver electricity to any specific customer or point of delivery.

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The total preliminary cost estimate to interconnect the 42 MW
the section of the section of the 138kV line is \$8,827,230 (See Table 1
Conceptual-Level Cost Estimate for GI #562) and includes the following tasks:
<ul> <li>New GI #562 138kV Generation Interconnection Station.</li> </ul>
• Rebuild of the approximately 69 kV line using
(or equivalent) conductor.
<ul> <li>Move approximately of the shared</li> </ul>
230kV structures near Caldwell. Utilize the old
69kV right of way for the re-located line
• Open-Breaker Transfer Trip Scheme.

The cost estimate includes direct equipment and installation labor costs, indirect labor costs and general overheads. The estimate does include a contingency allowance. These are cost estimates only and final charges to the customer will be based on the actual construction costs incurred. It should be noted that the preliminary cost estimate of \$8,827,230 does not include the cost of the customer's owned equipment to construct the solar generation site or required communication circuits.

Idaho Power transmission system upgrades might be required for projects ahead in the queue of this project, GI #562. In the scenario that a project(s) in the queue prior to this project withdraws or falls out of the queue, the feasibility study for this project will need to be re-evaluated and potentially re-studied. This may result in required additional system upgrades for GI #562.

## 3.0 Scope of Interconnection Feasibility Study

The Interconnection Feasibility Study was done and prepared in accordance with Idaho Power Company Standard Generator Interconnection Procedures to provide a preliminary evaluation of the feasibility of the interconnection of the proposed generating project to the Idaho Power system. As listed in the Interconnection Feasibility Study agreement, the Interconnection Feasibility Study report provides the following information:

- preliminary identification of any circuit breaker short circuit capability limits exceeded because of the interconnection;
- preliminary identification of any thermal overload or voltage limit violations resulting from the interconnection; and
- preliminary description and non-binding estimated cost of facilities required to interconnect the Large Generating Facility to the IPC system and to address the identified short circuit and power flow issues.

All other proposed generation projects prior to the Project in IPC's and Bonneville Power Administration's (BPA's) Generator Interconnect queues were considered in this study. A current list of IPC's projects can be found in the Generation Interconnection folder located on the Idaho Power web site at the link shown below:

## http://www.oatioasis.com/ipco/index.html.

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6.0 Description of Proposed Generating Project	
The proposed , GI #562, consists solar plant which requested to be connected to IPC's 138kV line at the approximate coordinate loc.  The Project's Commercial Operation Date (	ation of the
The single line diagram shows a GSU connected on Delta on on the generator side, this connection is not allowed and wou will need to provide a ground source, this is typically achieve grounded wye – grounded wye with a delta tertiary connection	ld need to be corrected. The projected, but not limited to, with a
7.0 Description of Substation Facilities	
The interconnection of GI #562, to the installation of an additional 138kV circuit breaker to alleviate 138kV line is already a three-terminal not allow another tap on this line and create a four-terminal li relaying issues. From a transmission system perspective, it was this additional 138kV sectionalizing breaker, would be to install looking toward looking toward 138kV line and a 138kV line and a	e protective relaying issues. The line. It is Idaho Power's policy to ne due to technical protective as determined the best location, for

### 8.0 Description of Transmission Facilities

The Project's impact on the Idaho-Northwest transmission path (WECC Path #14) and Brownlee East transmission path (WECC Path #55) were evaluated in this Generation Feasibility Study. The Idaho-Northwest transmission path was studied at both its West-to-East 1200 MW and East-to-West rated transfer capabilities. The Brownlee East transmission path was studied at its 1915 MW rated West-to-East transfer capability.

The Idaho-Northwest transmission path (WECC Path #14) is defined as the sum of the flows on the following five lines:

- Oxbow-Lolo 230kV
- Hells Canyon-Hurricane 230kV
- North Powder-La Grande 230kV
- Hines-Harney 115kV
- Hemingway-Summer Lake 500kV

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agreement with Idaho Power Company and have a need to know.

The Brownlee East transmission path (WECC Path #55) is defined as the sum of the flows on the following seven lines:

- Brownlee-Boise Bench #1 230kV
- Brownlee-Boise Bench #2 230kV
- Brownlee-Boise Bench #3 230kV
- Brownlee-Horse Flat #4 230kV
- Brownlee-Ontario 230kV
- Oxbow-Starkey 138kV
- Quartz-Ontario 138kV

For this generation interconnection Feasibility Study, the flow on the Path 14 Idaho-Northwest transmission path was modeled at 1200 MW West-to-East and the Brownlee East transmission path was modeled at 1915 MW West-to-East. The paths were stressed to these specific levels to determine if the addition of the Project's 42 MW degraded the existing Brownlee East path's transfer capability.

And, a Path 14 Idaho-Northwest study was performed to determine the Project's 42 MW potential impact on Path 14 Idaho-Northwest West-to-East rating of 1200 MW.

In addition to the Path 55 Brownlee East and Path 14 Idaho-Northwest West-to-East transmission paths studies, a Path 14 East-to-West sensitivity study was performed to determine the Project's 42 MW potential impact on Path 14 Idaho-Northwest East-to-West rating of 2400 MW.

### 9.0 Description of Power Flow Cases

For this Generation Interconnection Feasibility Study, two power flow cases (without and with the Project) were used to evaluate the potential impacts due to the 42 MW Grand, GI #562.

For the Path 14 Idaho-Northwest West-to-East 1200 MW transfer path rating impact study due to the addition of the Project, the WECC 2019 Heavy Summer case was chosen as the power flow base case. These cases were modified to stress the Idaho-Northwest transmission path West-to-East flows to 1200 MW simultaneous with the Brownlee East transmission path modeled at 1915 MW to determine the potential impact due to the addition of the 42 MW Project.

## 9.1 Power Flow Analysis Results

Results from the Path 14 Idaho-Northwest West-to-East 1200 MW transfer path rating impact study case indicate the addition of the GI #562 project will result in violations that need to be mitigated.

a. This contingency results in a post-transient overload violating the emergency rating of the 230kV lines, which requires network upgrades.

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b.	This contingency results in a rating of the	ost-transient overload violating the emergency 138kV line, which requires network		
c.	upgrades. This contingency results in a rating of the network upgrades	post-transient overload	-	
a.	This contingency results in a rating of the upgrades.	post-transient overload 69kV li	l violating the emergency ne, which requires network	
b.	This contingency results in a rating of the	post-transient overload 230 kV line, which	requires network upgrades.	
a.	This contingency results in a rating of the upgrades.	post-transient overload	violating the emergency ne, which requires network	
a.  5. The br a.	This contingency results in a rating of the upgrades. eaker failure in This contingency results in a rating of the upgrades.	69kV li	ne, which requires network	
Therefore, a subsequently (	Open-Breaker Transfer TGI #562 generation.	transformer and the	ng GI562 generation results 69 kV line. plemented to trip the line and	
The fault duty	at and breakers	without the Project mo	odeled are as follows.	
	Fault Study (w/o			
Location	······································	LTL (A)	3PH (A)	
	3331.0 1199.1	3780.3 1566.6	4426.6 1794.1	

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The fault duty at and the approximate POI breakers with the Project modeled are as follows.

Name of the State	Fault Study (w/	<b>1</b>	
Location	SLG (A)	LTL (A)	3PH (A)
	4252.8	3763.9	4406.8
	3667.4	2155.0	1307.0
	1389.0	1693.5	1681.5

The fault current contribution from the 42 MW PV facility does not exceed any circuit breaker rating.

The 138/34.5kV GSU transformer does <u>not</u> meet Idaho Power's transmission interconnection grounding requirements for system protection which requires a ground source on the high-side of the transformer. This can be typically achieved with an auto-transformer with a delta tertiary which is a source of ground current, (other configurations can and do exist). Refer to Appendix A, Section 3, for additional grounding requirements.

## 11.0 Description of Required Facility Upgrades

The Project will be required to provide a plant to regulate voltage according to a voltage schedule that will be provided by Idaho Power.

The following upgrades will be required to IPC-owned facilities to facilitate the interconnection of GI #562:

- New GI #562 138kV Generation Interconnection Station.
- Rebuild of the approximately conductor. 69 kV line using
- Move approximately 230kV structures near Caldwell. Utilize the old 69kV right of way for the re-located line
- Open-Breaker Transfer Trip Scheme.

See the conceptual-level cost estimate in Table 1.

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Table 1 Conceptual-Level Cost Estimate for GI #562

GI #562 Network Resource Generation Interconnection Facilities	
	Cost
GI #562 Generation Interconnection Station	\$2,842,000
Rebuild of 69 kV line	\$ 1,154,200
Move 230 kV structures. 138 kV line from	\$2,766,600
Open-Breaker Transfer Trip Scheme	TBD
Subtotal	\$6,762,800
Contingency (1)	\$1,352,560
Subtotal	\$8,115,360
Overheads (2)	\$711,870
Network Resource Generation Interconnection Facilities Total Conceptual-level Cost Estimate in 2020 dollars (3)	\$8,827,230

<sup>(1)</sup> Contingency is added to cover the unforeseen costs in the estimate. These costs can include unidentified design components, material cost increases, labor estimate shortfalls, etc.

(2) Overhead costs cover the indirect costs associated with the Project.

(3) This cost estimate includes direct equipment, material, labor, and overheads as shown.

- Note that these estimates do not include the cost of the customer's equipment/facilities or required communication circuits for SCADA, and metering.
- Note that the overhead rates are subject to change during the year.
- These are estimated costs only and final charges to the customer will be based on the actual construction costs incurred.
- These are non-binding conceptual level cost estimates that will be further refined upon the request and completion of Transmission Facility Study.

## 12.0 Description of Operating Requirements

It is the generation project's responsibility to provide reactive power capability of the project to have a power factor operating range of at least 0.95 leading (absorbing) to at least 0.95 lagging (supplying) at the POI over the range of real power output (up to maximum output of the project). Assuming inverters with a power factor operating range of 0.9 lagging (supplying) at

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maximum output, the 0.95 lagging (supplying) reactive power capability at the POI cannot be achieved without additional shunt reactive support.

The 6 MVAr 34.5kV shunt capacitor indicated on the Project's supplied single line drawing is sufficient to make-up the reactive power deficiency.

Identification of any additional equipment required at the plant to meet Idaho Power reactive power capability interconnection requirements will be provided in the Transmission System Impact Study if the generation interconnection customer chooses to move to the next study phase of the interconnection process.

The inverter(s) will be required to have the UL 1741SA certification prior to the installation and be approved by Idaho Power cybersecurity group.

The Project will be required to control voltage in accordance with a voltage schedule as provided by Idaho Power Grid Operations. Therefore, GI #562 will be required to install a plant controller for managing the real and reactive power output of the 42 MW inverter array at the project POI.

Voltage flicker at startup and during operation will be limited to less than 5% as measured at the POI. The allowable voltage flicker limit is further reduced during operation due to multiple voltage fluctuations per hour or minute, per Idaho Power's T&D Advisory Information Manual.

The Project is required to comply with the applicable voltage fluctuation limits found in IEEE Standard 1453-2004 *IEEE Recommended Practice for Measurement and Limits of Voltage Fluctuations and Associated Light Flicker on AC Power Systems*.

The project is required to comply with the applicable Voltage and Current Distortion Limits found in IEEE Standard 519-2014 *IEEE Recommended Practices and Requirements for Harmonic Control in Electrical Power Systems*.

Installation of phasor measurement unit devices at the POI and maintenance costs associated with communication circuits needed to stream PMU data will also be required to be provided to interconnect GI #562. The specific costs associated with the IPC requirements for interconnection customers with aggregate facilities larger than 20 MW to provide PMU data to IPC will be identified in the Facility Study should the generation interconnection customer choose to proceed to that phase of the interconnection process.

Any operating requirements for the Project may be identified in the Transmission System Impact Study when it is performed.

#### 13.0 Conclusion

The requested interconnection of the section of the section of the 138kV line was studied.	r's
The results of this study work confirm that it is feasible to interconnect the 42 MW Grand	

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A Transmission System Impact Study is required to determine the specific transmission network upgrades required to integrate the project as a Network Resource and to evaluate the system impacts such as thermal overload, voltage, transient stability, and reactive margin.

All generation projects in the area ahead of the Project in IPC's/BPA's generation interconnection queue and their associated transmission system improvements were modeled in a preliminary power flow analysis to evaluate the feasibility of interconnecting GI #562. The results and conclusions of this feasibility study are based on the realization of these projects in the unique queue/project order.

The estimated cost to interconnect GI #562 to the IPC system at the 138kV point of interconnection considered in this study is approximately \$8,827,230.

Generator interconnection service, either as an Energy Resource or a Network Resource, does not in any way convey any right to deliver electricity to any specific customer or point of delivery. Transmission requirements to integrate the Project will be determined during the Transmission System Impact Study phase of the generator interconnection process.

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#### APPENDIX A

#### A-1.0 Method of Study

The Feasibility Study plan inserts the Project up to the maximum requested injection into the selected Western Electricity Coordinating Council (WECC) power flow case and then, using Power World Simulator or GE's Positive Sequence Load Flow (PSLF) analysis tool, examines the impacts of the new resource on Idaho Power's transmission system (lines, transformers, etc.) within the study area under various operating and outage scenarios. The WECC and Idaho Power reliability criteria and Idaho Power operating procedures were used to determine the acceptability of the configurations considered. The WECC case is a recent case modified to simulate stressed but reasonable pre-contingency energy transfers utilizing the IPC system. For distribution feeder analysis, Idaho Power utilizes DNV·GL's Synergi Electric software and EPRI's OpenDSS software.

#### A-2.0 Acceptability Criteria

The following acceptability criteria were used in the power flow analysis to determine under which system configuration modifications may be required:

The continuous rating of equipment is assumed to be the normal thermal rating of the equipment. This rating will be as determined by the manufacturer of the equipment or as determined by Idaho Power. Less than or equal to 100% of continuous rating is acceptable.

Idaho Power's Voltage Operating Guidelines were used to determine voltage requirements on the system. These states, in part, that distribution voltages, under normal operating conditions, are to be maintained within plus or minus 5% (0.05 per unit) of nominal everywhere on the feeder. Therefore, voltages greater than or equal to 0.95 pu voltage and less than or equal to 1.05 pu voltage are acceptable.

Voltage flicker during starting or stopping the generator is limited to 5% as measured at the point of interconnection, per Idaho Power's T&D Advisory Information Manual.

Idaho Power's Reliability Criteria for System Planning was used to determine proper transmission system operation.

All customer generation must meet IEEE 519 and ANSI C84.1 Standards.

All other applicable national and Idaho Power standards and prudent utility practices were used to determine the acceptability of the configurations considered.

The stable operation of the system requires an adequate supply of volt-amperes reactive (VAr or VArs) to maintain a stable voltage profile under both steady-state and dynamic system conditions. An inadequate supply of VArs will result in voltage decay or even collapse under the worst conditions.

Equipment/line/path ratings used will be those that are in use at the time of the study or that are represented by IPC upgrade projects that are either currently under construction or whose budgets have been approved for construction in the near future. All other potential future ratings 42 MW

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are outside the scope of this study. Future transmission changes may, however, affect current facility ratings used in the study.

### A-3.0 Grounding Guidance

IPC requires interconnected transformers on the distribution system to limit their ground fault current to 20 amps at the Point of Interconnection.

## A-4.0 Electrical System Protection Guidance

IPC requires electrical system protection per <u>Facility Connection Requirements</u> found on the Idaho Power Web site,

# $\underline{https://docs.idahopower.com/pdfs/BusinessToBusiness/FacConnReq.pdf}$

# A-5.0 WECC Coordinated Off-Nominal Frequency Load Shedding and Restoration Requirements

IPC requires frequency operational limits to adhere to WECC Under-frequency and Over-frequency Limits per the <u>WECC Coordinated Off-Nominal Frequency Load Shedding and Restoration Requirements</u> available upon request.

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#### APPENDIX B



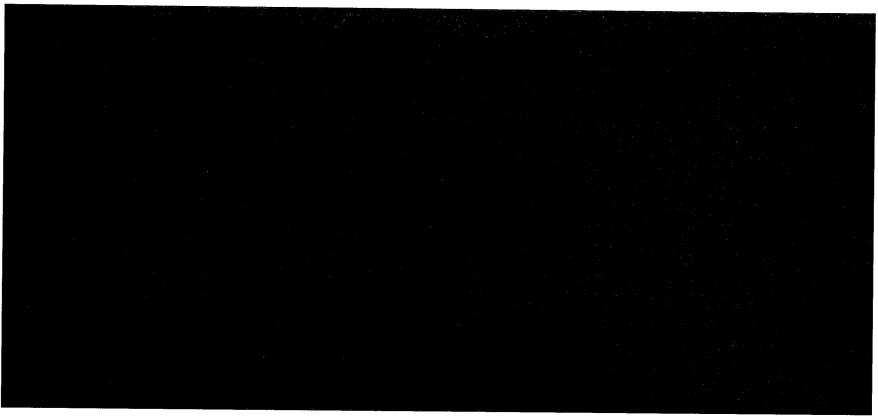


Figure 1 Location — GI #562

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